

MEMORANDUM

TO: Ananias Calvin, P.E.
Project Management Coordinator
Division of Highway Design

FROM: William Broyles, P.E.
Geotechnical Branch Manager
Division of Materials

BY: Danny Molen 
Geotechnical Branch

DATE: December 3, 2004

SUBJECT: **Oldham County**
FD52 093 0393 002-006 D
KY 393 from I-71 to KY 146
Station 330+85 to 401+00
Item # 5-234.00
Mars # 5941402D
Geotechnical Engineering Roadway Report

An abbreviated geotechnical engineering report is completed for the subject project. The Geotechnical Branch performed the drilling, sampling and testing. The purpose of the investigation was to define the soil and subsurface conditions. Reduced size geotechnical notes sheet, soil profile sheets, cut and embankment stability sheets are attached. The CADD input for these sheets is being e-mailed to the design consultant (Skees Engineering), as DGN files, for incorporation into the roadway plans.

The Select Rock Quantity Sheet was submitted by the design consultant. Based on these estimates, a sufficient quantity of limestone and/or durable shale will be available from roadway excavation on this project to perform all the following applicable notes requiring this material.

Stability analyses were performed at several locations, which indicated no problems to be expected with slopes constructed at 2:1 or flatter. The drawings are attached showing the results of these analyses.

Geotechnical recommendations are as follows:

- 1). In accordance with Section 206 of the current Standard Specifications, the moisture content of embankment material shall not vary from the optimum moisture content as determined by KM 64-511 by more than +2 percent or less than -2 percent. This moisture content requirement shall have equal weight with the density requirement when determining the acceptability of embankment construction. Refer to the Family of Curves for moisture/density correlation.
- 2). All soils, whether from roadway or borrow, may require manipulation to obtain proper moisture content prior to compaction. Direct payment shall not be permitted for rehandling, hauling, stockpiling, and/or manipulating soils.

- 3). Excavation of surface ditches and channel changes adjacent to embankment areas shall be performed prior to the placement of the adjacent embankments. The material excavated for the channel changes and surface ditches is suitable for embankment construction if dried to proper moisture content in accordance with Section 206 of the current Standard Specifications. Direct payment shall not be permitted for rehandling, hauling, stockpiling, and/or manipulating soils.
- 4). The contractor is responsible for conducting any operations necessary to excavate the cut areas to the required typical section. These operations shall be incidental to the roadway price.
- 5). The contractor shall conduct grading operations in such a manner that limestone from roadway excavation be stockpiled separately or otherwise manipulated so that ample quantities are available for those areas requiring said material. No direct payment will be allowed for such necessary manipulating as stockpiling, hauling and/or double handling the material.
- 6). The contractor shall conduct grading operations in such a manner that durable shale from roadway excavation be stockpiled separately or otherwise manipulated so that ample quantities are available for those areas requiring said material. No direct payment will be allowed for such necessary manipulating as stockpiling, hauling and/or double handling the material.
- 7). To provide a working platform for embankment construction, a sufficient thickness (estimated to be 3 ft) of limestone and/or durable shale from roadway excavation shall be placed over all soft and/or saturated foundation areas that may be detected during construction and/or to fill and stabilize the existing drains located within the limits of the roadway embankment construction, as directed by the Engineer. The placement of this material is incidental to the unit bid price for roadway excavation or embankment-in-place. The rock material shall be underlain with Geotextile Fabric, Type III, in accordance with Sections 214 & 843 of the current Standard Specifications. For estimation purposes only, the following areas are anticipated to require the above referenced treatment. Actual thickness and locations of the working platform will be determined by the Engineer during construction. The cost of placing the working platform shall be incidental to the unit price bid for roadway excavation (or embankment-in-place) and geotextile fabric. Wet areas were noted during the subsurface investigations at the following approximate locations:

Mainline

Station 391+25 to 391+75

Frontage Road

Station 144+60 to 145+10

- 8). The contractor shall construct foundation embankment benches and transverse benches as indicated on the plans and/or as directed by the Engineer, prior to placement of embankments in areas requiring such benches.
- 9). Transverse benching and/or perforated pipe underdrains shall be installed at the following approximate locations and any others designated by the Engineer. Contrary to Standard Drawing RDP-006, transverse benches and perforated pipe underdrains shall be placed on both the upgrade and downgrade cut to fill transitions.

Station 340+00

Station 350+50

Station 372+25

Station 382+40

10). Foundation embankment benches shall be placed in accordance with Standard Drawing RGX-010 at the locations listed below and/or as directed by the Engineer.

Ramp C-1

Station 9+00 to 10+25

Frontage Road

Station 143+75 to 144+75

CSXT Runaround

Station 2424+25 to 2428+75

11). The pond at the following location and any others designated by the Engineer shall be drained and any soft or saturated material shall be removed (approximately 2 feet). Use of this excavated material shall be limited to final dressing of roadway slopes, as directed by the Engineer. Approximately 2 feet of limestone and/or durable shale from roadway excavation may be required to stabilize the area. However, the actual thickness shall be determined by the Engineer. The placement of this material is incidental to the unit bid price for roadway excavation or embankment-in-place.

Station 346+50

12). Shale (above or below the RDZ, durable or nondurable) cannot be used in the subgrade.

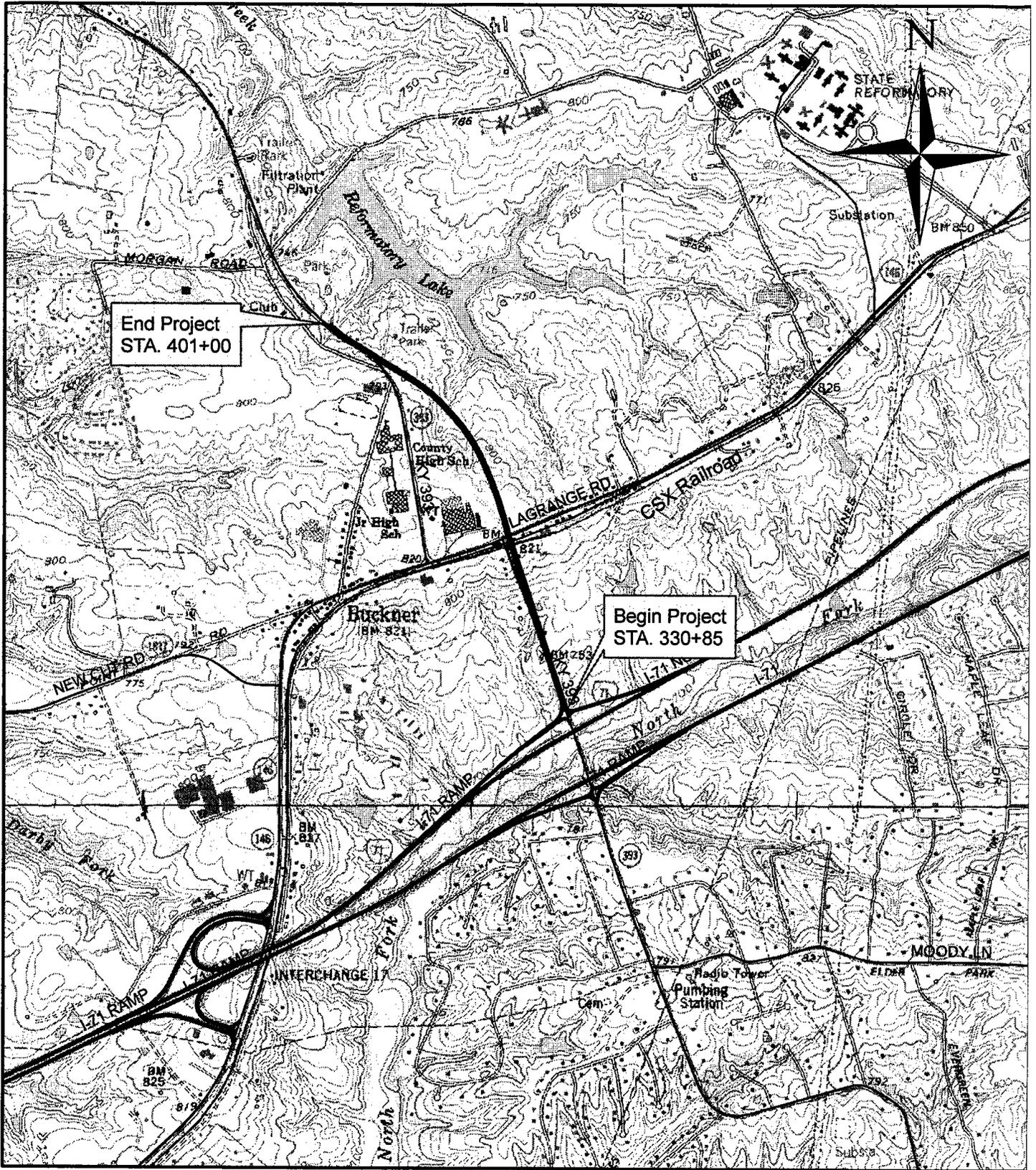
DESIGN RECOMMENDATIONS . . .

1). The project should be designed for a 2 foot rock roadbed. A CBR design value of 11.0 is recommended for the rock, and a CBR design value of 2.0 is recommended for the soil beneath the rock. The rock shall consist of limestone from roadway excavation. The placement of this material is incidental to the unit bid price for roadway excavation or embankment-in-place.

cc: Kentucky Transportation Center
Division of Design (Plan Processing Section)
TEBM for Pavement Design
Division of Construction
TEBM for Construction (District) 2 copies
TEBM for Preconstruction (District)
Skees Engineering

Attachments

OLDHAM COUNTY - KY 393



1:24,000

**OLDHAM COUNTY
KY 393
FROM I-71 TO NORTH OF KY 146
ITEM # 5-340.00
MARS # 5941402D**

GEOTECHNICAL SYMBOL SHEET

COUNTY OF	ITEM NO.	SHEET NO.
OLDHAM	5-234.0	

AASHTO Classification of Soils and Soil-Aggregate Mixtures

General Classification	Granular Materials (35% or less passing 0.075 mm)						Silt-Clay Materials (More than 35% passing 0.075 mm)			
	A-1		A-3	A-2			A-4	A-5	A-6	A-7
	A-1-a	A-1-b		A-2-4	A-2-5	A-2-6				
Sieve Analysis, Percent Passing										
2.00 mm (No. 10)	50 max	---	---	---	---	---	---	---	---	---
0.425 mm (No. 40)	30 max	50 max	51 min	---	---	---	---	---	---	---
0.075 mm (No. 200)	15 max	25 max	10 max	35 max	35 max	35 max	35 max	36 min	36 min	36 min
Characteristics of Fraction Passing 0.425 mm (No. 40)										
Liquid Limit	---	---	---	40 max	41 min	40 max	41 min	40 max	41 min	40 max
Plasticity Index	6 max	---	N.P.	10 max	10 max	11 min	11 min	10 max	10 max	11 min

Unified Soil Classifications

MAJOR DIVISIONS	SYMBOL	NAME	
COARSE GRAINED SOILS	GRAVEL AND GRAVELLY SOILS	GW 	Well-graded gravels or gravel-sand mixtures, little or no fines.
		GP 	Poorly graded gravels or gravel-sand mixtures, little or no fines.
		GM 	Silty gravels, gravel-sand-silt mixtures.
		GC 	Clayey gravels, gravel-sand-clay mixtures.
	SAND AND SANDY SOILS	SW 	Well graded sands or gravelly sands, little or no fines.
		SP 	Poorly graded sands or gravelly sands, little or no fines.
		SM 	Silty sands, sand-silt mixtures.
		SC 	Clayey sands, sand-clay mixtures.
FINE GRAINED SOILS	SILTS AND CLAYS LL IS LESS THAN 50	ML 	Inorganic silts and very fine sands, rock flour, silty or clayey fine sands or clayey silts with slight plasticity.
		CL 	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays.
	SILTS AND CLAYS LL IS GREATER THAN 50	MH 	Inorganic silts, micaceous or diatomaceous fine sandy or silty soils, elastic silts.
		CH 	Inorganic clays of high plasticity, fat clays.
UNCLASSIFIED MATERIAL	NONE	Non-classified material (i.e. overburden, pavement, slag, etc.) Include visual description.	

- AI Activity Index
 - LI Liquidity Index
 - S+C Silt + Clay (% finer than No.200 Sieve)
 - Rockline Soundings
 - ⊕ Disturbed Sample Boring
 - ⊙ Undisturbed Sample Boring
 - ⊗ Undisturbed Sample Boring & Rock Core
 - Rock Core
 - ⊗ Slope Inclinator Installation
- typical applications:
- OW Observation Well
 - ➔ Approximate Footing Elevation
 - ▼ (Date) Water Elevation
 - VS (psf) Field Vane Shear Strength
 - Thin-walled Tube Sample
 - < Standard Penetration Test Sample
 - N Penetration Resistance
 - Qu (psf) Unconfined Compressive Strength
 - UU (psf) Unconsolidated Undrained Triaxial Strength
 - w% Moisture Content
 - KY RQD Rock Quality Designation (Kentucky Method)
 - STD RQD Rock Quality Designation (Standard Method)
 - SDI(JS) Slake Durability Index (Jar Slake Test)
 - REC Core Recovery
 - ∅ Angle of Internal Friction (Total Stress)
 - ∅̄ Angle of Internal Friction (Effective Stress)
 - c (psf) Cohesion (Total Stress)
 - c̄ (psf) Cohesion (Effective Stress)
 - γ (pcf) Total Unit Weight
 - RDZ Rock Disintegration Zone
 - OB Overburden Bench
 - IB Intermediate Bench
 - R Refusal
 - NR Refusal Not Encountered

- LIMESTONE
- SANDSTONE
- DURABLE SHALE (SDI ≥ 95)
- NONDURABLE SHALE (SDI < 95)
- COAL
- TALUS, MINE WASTE, FILL MATERIAL, BOULDERS, & ETC.
- GRANULAR EMBANKMENT
- STRUCTURE GRANULAR BACKFILL
- SLOPE PROTECTION

CHECKED BY _____ DATE _____
 APPROVED BY _____ DATE _____
 DD-MMM-YYYY HH:MM

GEOTECHNICAL NOTES

COUNTY OF	ITEM NO.	SHEET NO.
OLDHAM	5-234.0	

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<u>Mainline</u>	<u>Frontage Road</u>
Station 391+25 to 391+75	Station 144+60 to 145+10

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Station 340+00
 Station 350+50
 Station 372+25
 Station 382+40

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Station 9+00 to 10+25	Station 143+75 to 144+75	Station 2424+25 to 2428+75

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Station 346+50

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**KENTUCKY
 DEPARTMENT OF HIGHWAYS
 COUNTY OF
 OLDHAM**

PROJECT _____
 NUMBERS _____

GEOTECHNICAL NOTES

CHECKED BY _____ DATE _____
 APPROVED BY _____ DATE _____

UD-MMM-1111 PER. MM

Field Drilling and Sampling were performed in the period of MAY 20 04 to JUNE 20 04.

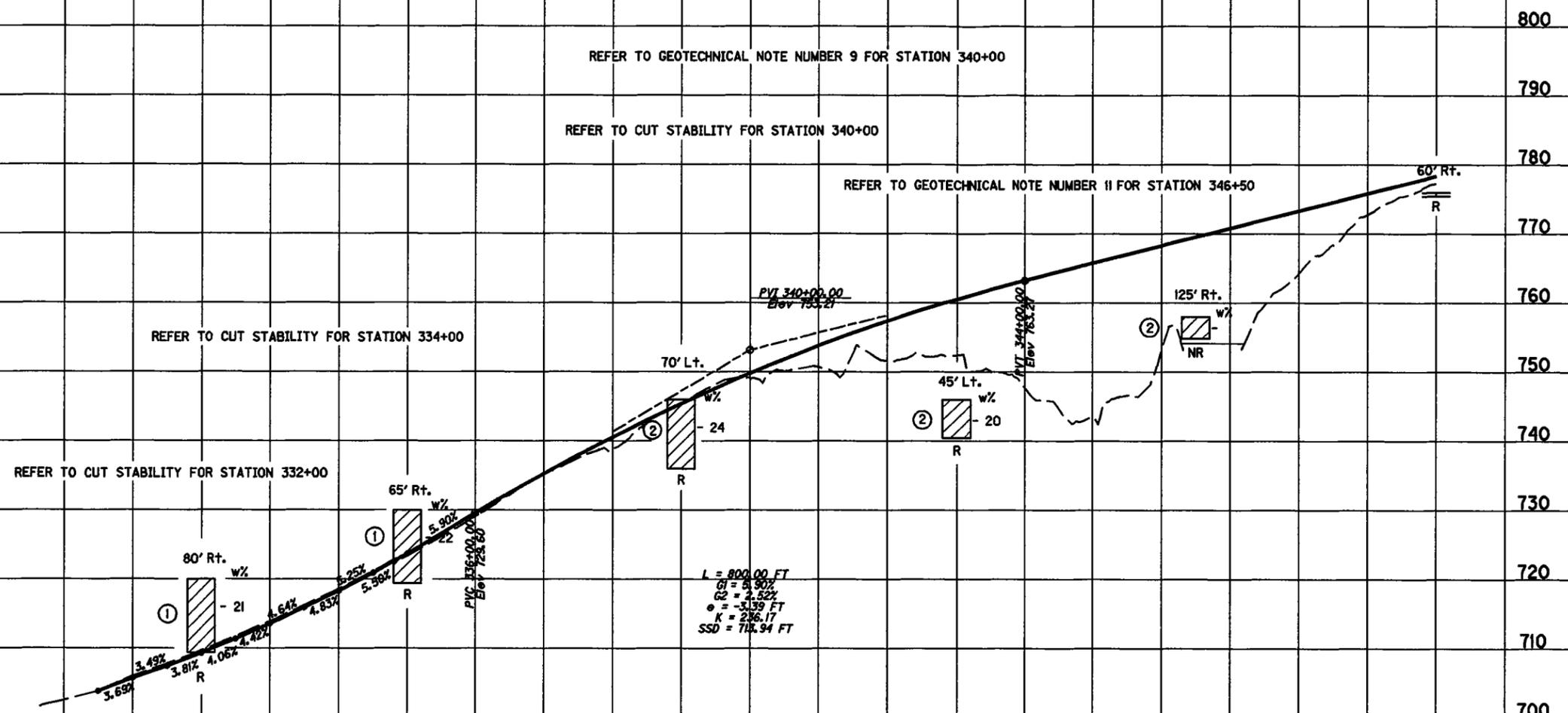
Detailed data and interpretation of subsurface conditions encountered in individual borings are shown on the soil profile. Soil and rock strata descriptions and indicated boundaries are based on engineering interpretation of available subsurface information obtained at selected locations, and may not necessarily reflect the actual variation in subsurface conditions between borings and samples.

The observed water levels and/or subsurface conditions indicated on the soil profile are as recorded at the time of exploration. These water levels and/or subsurface conditions may vary considerable with time, according to the prevailing climate, rainfall or other factors and are otherwise dependent on the duration of and methods used in the exploration program.

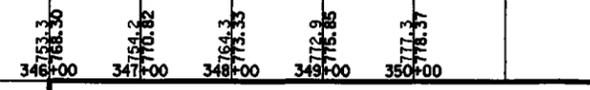
Selected rock cores and all applicable drill logs, are stored at the Division of Materials in Frankfort and are available for inspection on request. Contact the Division of Materials, Geotechnical Branch for availability information and to schedule an inspection.

NOTICE - Without regard to the materials encountered, all roadway and drainage excavation shall be unclassified and shall be designated as Roadway Excavation. It shall be distinctly understood that any reference to rock, earth or any other materials on the plans or cross sections whether in numbers, words, letters, or lines, is solely for the Department's information and is not to be taken as an indication of classified excavation or the quantity of either rock, earth or any other material involved.

The bidder must draw his own conclusions as to the conditions to be encountered. The Department does not give any guarantee as to the accuracy of the data and no claim will be considered for additional compensation when the materials encountered are not in accord with the classification shown.



SAMPLE NO.	1	2
STATION	332+00	339+00
OFFSET	80' Rt.	70' Lt.
DEPTH	0.0-10.5	0.0-10.0
COMPOSITION OF TOTAL SAMPLE	GRAVEL (- 3" + NO. 10)	0
	SAND (- NO 10 + NO. 200)	11
	SILT (- 0.075 mm + 0.002 mm)	51
	CLAY (- 0.002 mm)	38
LIQUID LIMIT	32	38
PLASTIC LIMIT	21	21
PLASTICITY INDEX	11	17
ACTIVITY INDEX	.29	.39
SPECIFIC GRAVITY	2.74	2.77
AASHTO CLASSIFICATION	A-7-6(9)	A-6(16)
UNIFIED CLASSIFICATION	CL	CL
CALIFORNIA BEARING RATIO	3.2	1.6
MAXIMUM DRY DENSITY (pcf)	110	104
OPTIMUM MOISTURE (%)	18	20
Z +4.75mm MATERIAL IN CBR & MOISTURE-DENSITY TESTS	-	-



**KENTUCKY
DEPARTMENT OF HIGHWAYS
COUNTY OF
OLDHAM**

PROJECT _____
NUMBERS _____

**SOIL PROFILE, KY 393
STA. 330+00 TO 350+00**

CHECKED BY _____ DATE _____
 APPROVED BY _____ DATE _____
 Cell Name: ssp
 DD-MMM-YYYY HH:MM

REFER TO CUT STABILITY FOR STATION 356+50

REFER TO CUT STABILITY FOR STATION 353+50

REFER TO CUT STABILITY FOR STATION 361+00

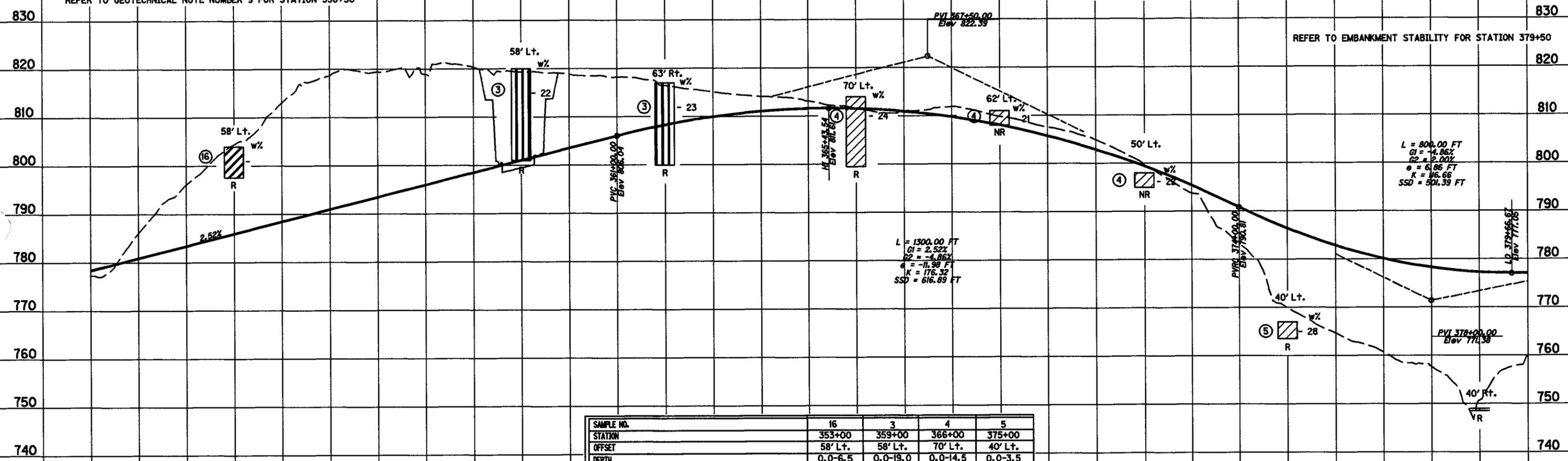
REFER TO CUT STABILITY FOR STATION 357+00

REFER TO CUT STABILITY FOR STATION 367+50

REFER TO GEOTECHNICAL NOTE NUMBER 9 FOR STATION 350+50

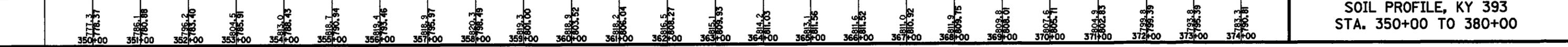
REFER TO GEOTECHNICAL NOTE NUMBER 9 FOR STATION 372+50

REFER TO EMBANKMENT STABILITY FOR STATION 379+50



SAMPLE NO.	16	3	4	5
STATION	353+00	359+00	366+00	375+00
OFFSET	58' Lt.	58' Lt.	70' Lt.	40' Lt.
DEPTH	0.0-6.5	0.0-19.0	0.0-14.5	0.0-3.5
COMPOSITION OF TOTAL SAMPLE	GRAVEL (- 3" + NO. 10)	0	0	3
	SAND (- NO 10 + NO. 200)	4	3	4
	SILT (- 0.075 mm + 0.002 mm)	44	17	38
	CLAY (- 0.002 mm)	52	80	58
LIQUID LIMIT	51	65	48	36
PLASTIC LIMIT	27	37	25	23
PLASTICITY INDEX	24	28	23	13
ACTIVITY INDEX	.46	.35	.39	.36
SPECIFIC GRAVITY	2.68	2.77	2.63	2.63
AASHTO CLASSIFICATION	A-7-6(27)	A-7-5(35)	A-7-6(25)	A-6(12)
UNIFIED CLASSIFICATION	CH	MH	CL	CL
CALIFORNIA BEARING RATIO	2.7	1.4	3.6	3.9
MAXIMUM DRY DENSITY (pcf)	99	90	95	100
OPTIMUM MOISTURE (C)	23	29	25	22
% +4.75mm MATERIAL IN CBR & MOISTURE-DENSITY TESTS	-	-	-	-

PREPARED BY _____ DATE _____
 CHECKED BY _____ DATE _____
 APPROVED BY _____ DATE _____

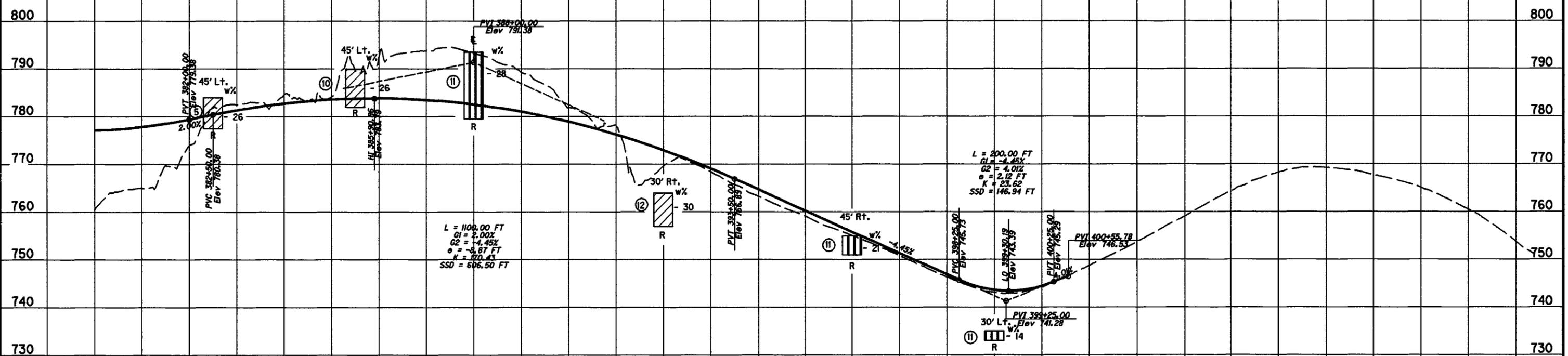


SOIL PROFILE, KY 393
 STA. 350+00 TO 380+00

REFER TO GEOTECHNICAL NOTE NUMBER 9 FOR STATION 382+40

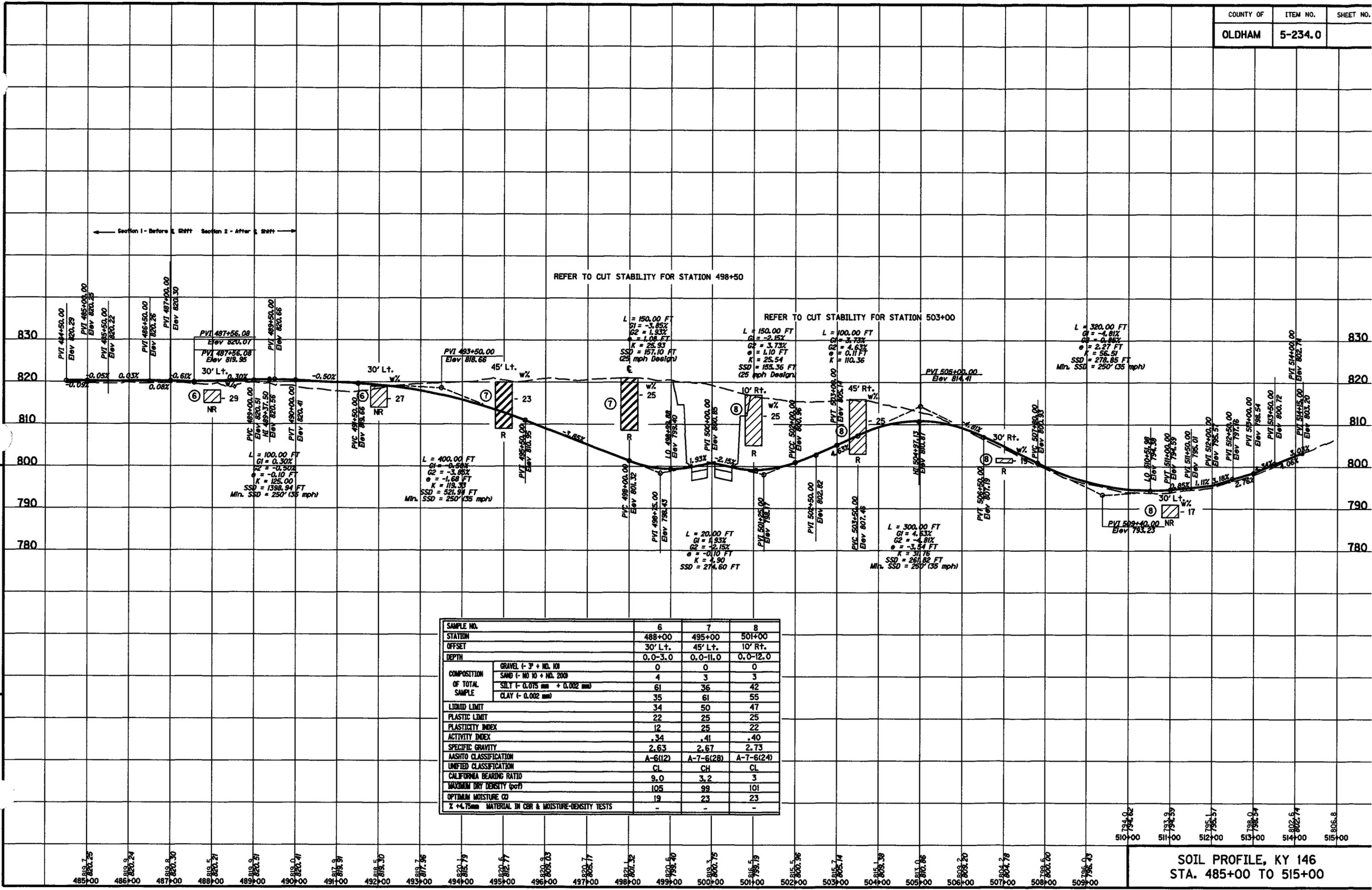
REFER TO GEOTECHNICAL NOTE NUMBER 7 FOR STATION 391+25 TO 391+75

REFER TO CUT STABILITY FOR STATION 387+50



SAMPLE NO.	5	10	11	12
STATION	375+00	385+50	388+80	392+00
OFFSET	40' Lt.	45' Lt.	0	30' Rt.
DEPTH	0.0-3.5	0.0-8.0	0.0-14.0	0.0-7.0
COMPOSITION OF TOTAL SAMPLE	GRAVEL (- 3 + NO. 10)	3	10	1
	SAND (- NO 10 + NO. 200)	10	18	7
	SILT (- 0.075 mm + 0.002 mm)	51	39	25
	CLAY (- 0.002 mm)	36	33	66
LIQUID LIMIT	36	32	56	36
PLASTIC LIMIT	23	20	30	21
PLASTICITY INDEX	13	12	26	15
ACTIVITY INDEX	.36	.36	.39	.36
SPECIFIC GRAVITY	2.63	2.68	2.78	2.75
AASHTO CLASSIFICATION	A-6(12)	A-6(7)	A-7-5(28)	A-6(14)
UNIFIED CLASSIFICATION	CL	CL	MH	CL
CALIFORNIA BEARING RATIO	3.9	4.1	2.6	5.8
MAXIMUM DRY DENSITY (pcf)	100	107	94	113
OPTIMUM MOISTURE (%)	22	17	26	13
% +4.75mm MATERIAL IN CBR & MOISTURE-DENSITY TESTS	-	-	-	6

APPROVED BY DATE



PREPARED BY _____ DATE _____
 CHECKED BY _____ DATE _____
 APPROVED BY _____ DATE _____

SAMPLE NO.	6	7	8
STATION	488+00	495+00	501+00
OFFSET	30' Lt.	45' Lt.	10' Rt.
DEPTH	0.0-3.0	0.0-11.0	0.0-12.0
COMPOSITION OF TOTAL SAMPLE	GRAVEL (- 3" + NO. 10)	0	0
	SAND (- NO 10 + NO. 200)	4	3
	SILT (- 0.075 mm + 0.002 mm)	61	36
	CLAY (- 0.002 mm)	35	61
LIQUID LIMIT	34	50	47
PLASTIC LIMIT	22	25	25
PLASTICITY INDEX	12	25	22
ACTIVITY INDEX	.34	.41	.40
SPECIFIC GRAVITY	2.63	2.67	2.73
AASHTO CLASSIFICATION	A-6(12)	A-7-6(28)	A-7-6(24)
UNIFIED CLASSIFICATION	CL	CH	CL
CALIFORNIA BEARING RATIO	9.0	3.2	3
MAXIMUM DRY DENSITY (pcf)	105	99	101
OPTIMUM MOISTURE (%)	19	23	23
% +4.75mm MATERIAL IN CBR & MOISTURE-DENSITY TESTS	-	-	-

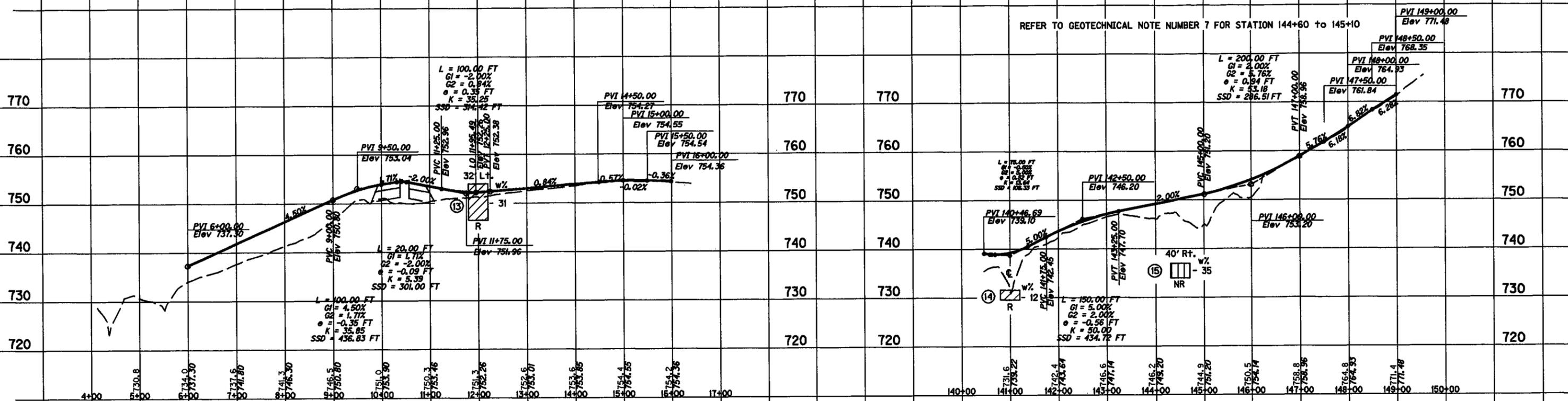
Cell Library: kyt.cel
 Cell Name: esp
 DD-MMM-YYYY HH:MM

794.82
794.39
795.57
798.94
802.97
806.8

SOIL PROFILE, KY 146
 STA. 485+00 TO 515+00

REFER TO GEOTECHNICAL NOTE NUMBER 10 FOR STATION 143+75 TO 144+75

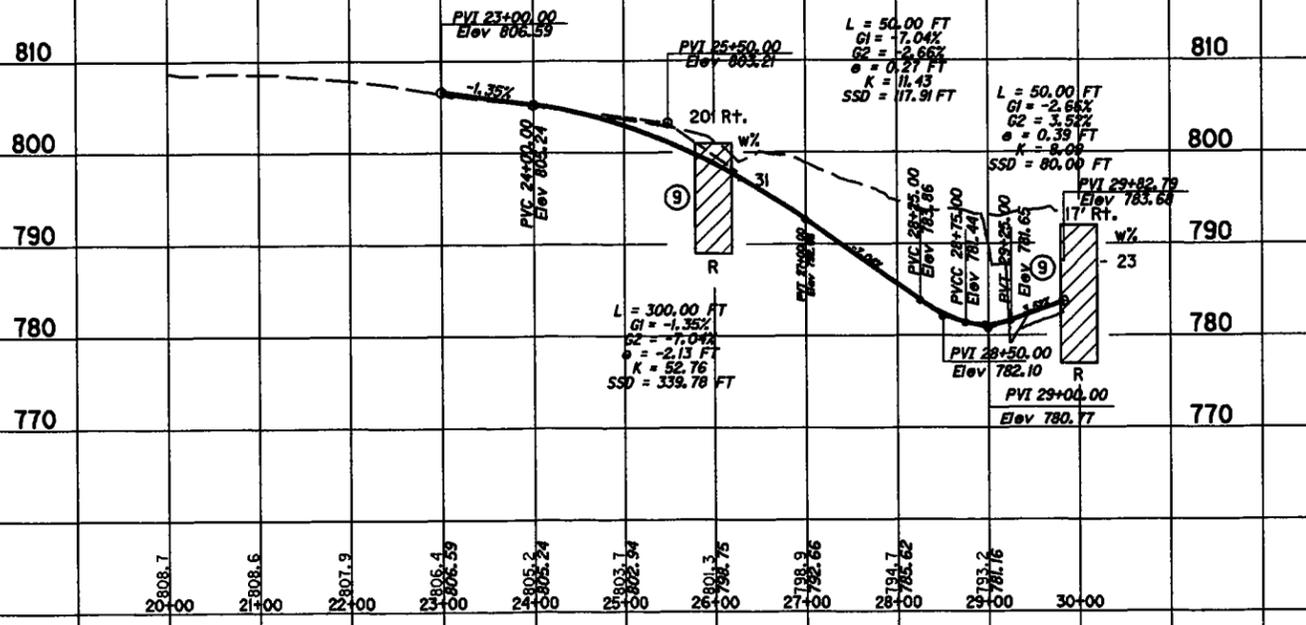
REFER TO GEOTECHNICAL NOTE NUMBER 7 FOR STATION 144+60 TO 145+10



SOIL PROFILE, COMMERCE PKWY. STA. 4+00 TO 17+00

SOIL PROFILE, FRONTAGE RD. STA. 140+00 TO 150+00

SAMPLE NO.	13	14	15	9
STATION	12+00	141+00	144+50	26+00
OFFSET	32' Lt.	0	40' Rt.	20' Rt.
DEPTH	0.0-7.5	0.0-2.0	0.0-3.0	0.0-12.0
COMPOSITION OF TOTAL SAMPLE	GRAVEL (- 3" + NO. 10)	0	4	5
	SAND (- NO 10 + NO. 200)	7	18	11
	SILT (- 0.075 mm + 0.002 mm)	51	47	54
	CLAY (- 0.002 mm)	42	31	30
LIQUID LIMIT	36	29	40	44
PLASTIC LIMIT	21	18	26	22
PLASTICITY INDEX	15	11	14	22
ACTIVITY INDEX	.35	.36	.47	.44
SPECIFIC GRAVITY	2.64	2.74	2.70	2.73
AASHTO CLASSIFICATION	A-6(14)	A-6(7)	A-6(12)	A-7-6(22)
UNIFIED CLASSIFICATION	CL	CL	ML	CL
CALIFORNIA BEARING RATIO	3.7	3.6	4.9	2.5
MAXIMUM DRY DENSITY (pcf)	106	118	96	101
OPTIMUM MOISTURE (%)	20	15	21	22
% +4.75mm MATERIAL IN CBR & MOISTURE-DENSITY TESTS	-	-	-	-



SOIL PROFILE, KY 393 CONN. STA. 20+00 TO 30+00

SOIL PROFILES, COMMERCE PKWY. FRONTAGE RD. & KY 393 CONNECTOR

CHECKED BY DATE
 APPROVED BY DATE
 DATE

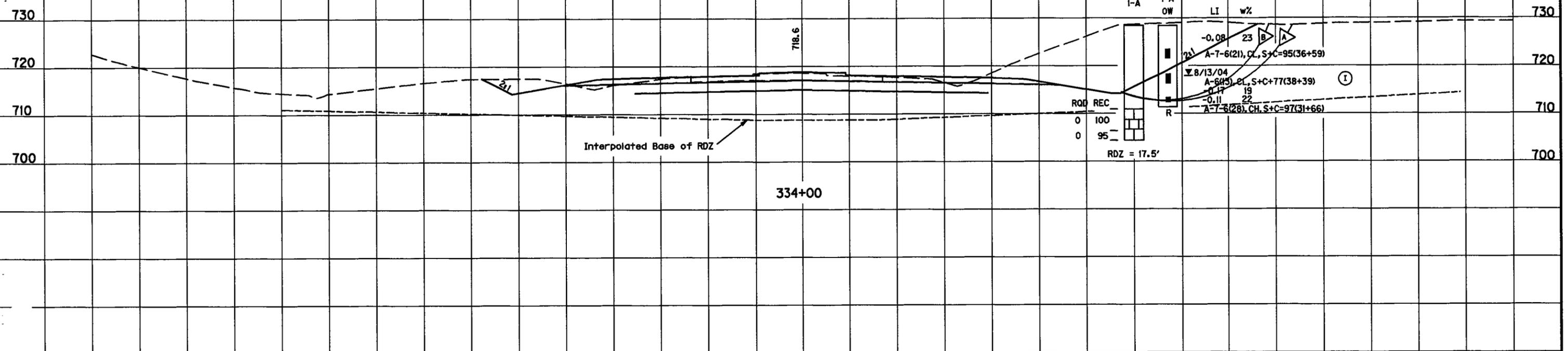
FACTORS OF SAFETY		
INTERMEDIATE TERM	A	2.0
LONG TERM	B	1.4

SUMMARY OF TRIAXIAL TEST DATA	
STATION	334+00
OFFSET	77' Rt.
DEPTH	10.0-12.0 15.0-16.0
$\bar{\sigma}$	195 psf
$\bar{\phi}$	28°

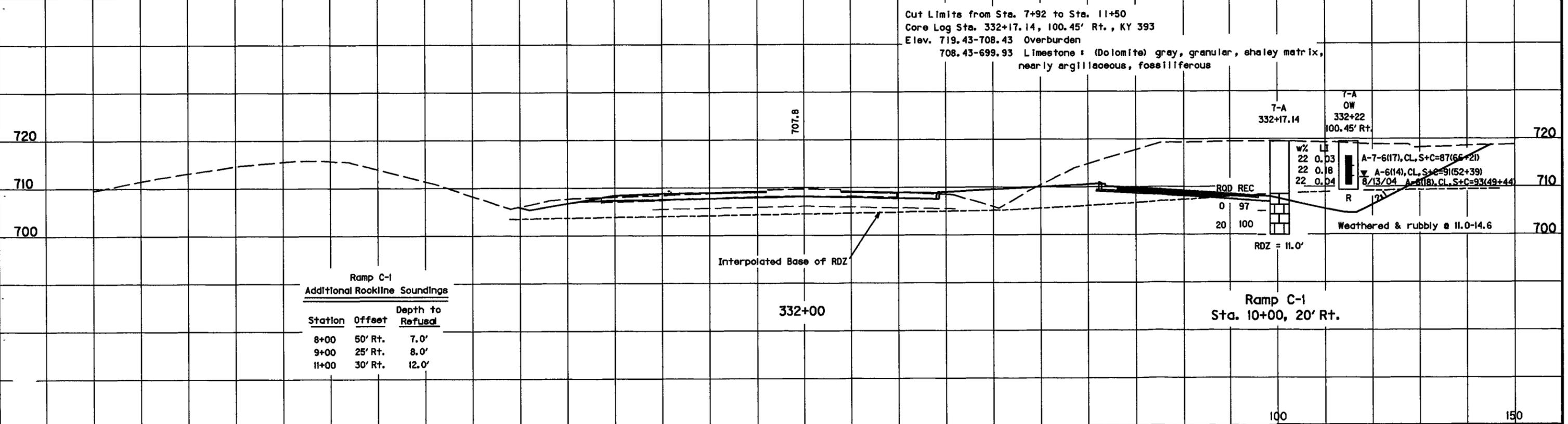
Additional Rookline Soundings		
Station	Offset	Depth to Refusal
333+00	75' Rt.	12.0'
335+00	65' Rt.	10.5'
336+00	70' Rt.	8.0'

Cut Limits from Sta. 331+50 to Sta. 336+50
 Core Log Sta. 334+00, 70' Rt.
 Elev. 728.43-710.93 Overburden
 710.93-704.43 Limestone: (Dolomite) gray, crystalline-granular, shaley matrix w/occasionally argillaceous partings & zones, fossiliferous

ASSUMED SOIL STRENGTH PARAMETERS	
SOIL	I
INTERMEDIATE TERM	\bar{c} = 125 psf $\bar{\phi}$ = 28°
LONG TERM	\bar{c} = 40 psf $\bar{\phi}$ = 28°



Cut Limits from Sta. 7+92 to Sta. 11+50
 Core Log Sta. 332+17.14, 100.45' Rt., KY 393
 Elev. 719.43-708.43 Overburden
 708.43-699.93 Limestone: (Dolomite) gray, granular, shaley matrix, nearly argillaceous, fossiliferous



Ramp C-1 Additional Rookline Soundings		
Station	Offset	Depth to Refusal
8+00	50' Rt.	7.0'
9+00	25' Rt.	8.0'
11+00	30' Rt.	12.0'

Ramp C-1
 Sta. 10+00, 20' Rt.

Additional Rockline Soundings

Station	Offset	Depth to Refusal
339+00	70' Lt.	10.0'

Cut Limits from Sta. 337+50 to Sta. 341+50

Core Log Sta. 340+14.5, 75' Lt.

Elev. 751.83-743.83 Overburden

743.83-742.53 Limestone : (Dolomite) gray, fine crystalline-granular, fossiliferous

742.53-739.63 Clay Soil filled void, fat clay w/rock frags & organics

739.63-734.83 Shale : gray, clayey-silty, ooliteous-dolomitic w/limestone partings near base

760

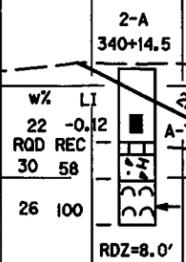
760

750

750

740

740



A-7-6(22), CL, S+C=9(37+54)

SDI(JS)
96 (5)

Vertical Water Stained
Joint @ 12.7-13.2

748.1

Interpolated Base of RDZ

340+00

100

150

150

100

50

0

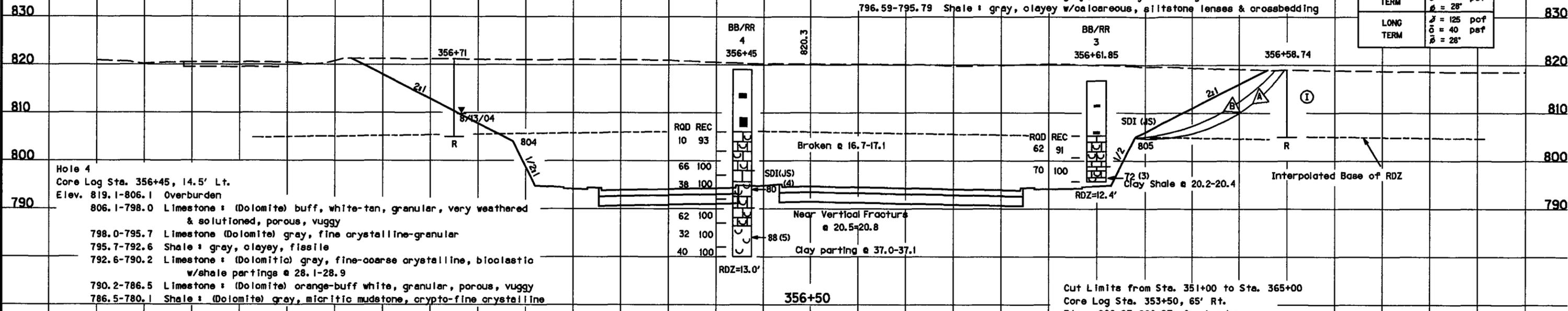
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DATE
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FACTORS OF SAFETY		
INTERMEDIATE TERM	A	2.0
LONG TERM	B	1.4

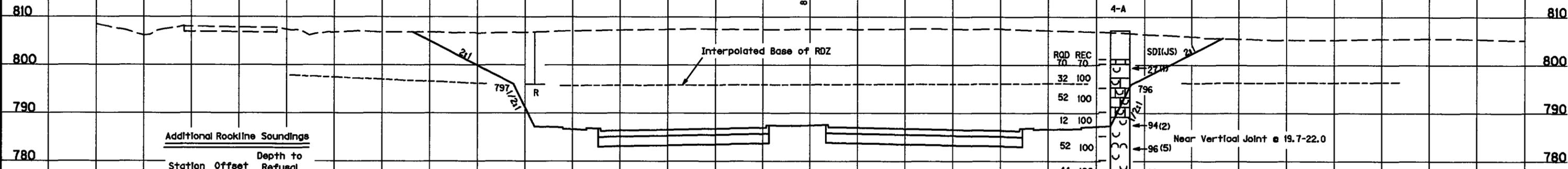
ASSUMED SOIL STRENGTH PARAMETERS	
SOIL	I
INTERMEDIATE TERM	$\phi = 125$ pcf $c = 200$ pcf $\delta = 28^\circ$
LONG TERM	$\phi = 125$ pcf $c = 40$ pcf $\delta = 28^\circ$

Hole 3
 Core Log Sta. 356+61.85, 60' Rt.
 Elev. 816.79-805.29 Overburden
 805.29-798.89 Limestone : (Dolomite) buff, white-tan, granular, very weathered & solutioned, porous
 798.89-796.59 Limestone (Dolomite) gray, fine crystalline-granular
 796.59-795.79 Shale : gray, clayey w/calcareous, siltstone lenses & crossbedding



Hole 4
 Core Log Sta. 356+45, 14.5' Lt.
 Elev. 819.1-806.1 Overburden
 806.1-798.0 Limestone : (Dolomite) buff, white-tan, granular, very weathered & solutioned, porous, vuggy
 798.0-795.7 Limestone (Dolomite) gray, fine crystalline-granular
 795.7-792.6 Shale : gray, clayey, fissile
 792.6-790.2 Limestone : (Dolomite) gray, fine-coarse crystalline, bioclastic w/shale partings @ 28.1-28.9
 790.2-786.5 Limestone : (Dolomite) orange-buff white, granular, porous, vuggy
 786.5-780.1 Shale : (Dolomite) gray, micritic mudstone, crypto-fine crystalline

Cut Limits from Sta. 351+00 to Sta. 365+00
 Core Log Sta. 353+50, 65' Rt.
 Elev. 806.27-799.27 Overburden
 800.27-799.27 Limestone : (Dolomite) brown, granular, weathered
 799.27-796.37 Shale : brown-gray, clayey, fissile
 796.37-788.27 Limestone : (Dolomite) gray, fine crystalline-granular w/limited shale partings
 788.27-773.07 Shale : gray, clayey-silty, occasionally fissile, w/calcareous mudstone siltstone partings & zones
 773.07-770.27 Limestone : (Dolomite) light gray, fine-coarse crystalline, fossiliferous, w/limited shale partings



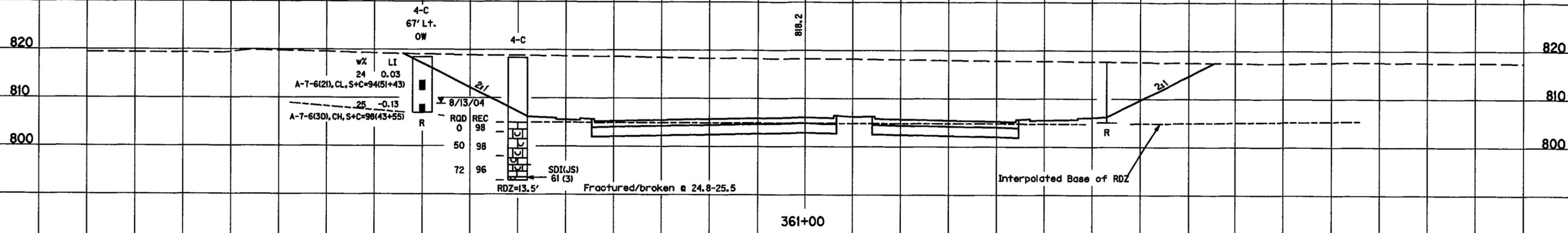
Additional Rookline Soundings

Station	Offset	Depth to Refusal
352+00	65' Rt.	5.5'
353+00	58' Lt.	6.5'
353+00	62' Rt.	5.5'
354+00	58' Lt.	9.5'
359+00	58' Lt.	10.0'
359+00	63' Rt.	13.5'
360+00	58' Lt.	12.0'
360+00	63' Rt.	13.5'
362+00	58' Lt.	16.5'
362+00	63' Rt.	17.0'
363+00	58' Lt.	14.0'
363+00	63' Rt.	14.0'
364+00	58' Lt.	15.5'

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 CHECKED BY _____
 APPROVED BY _____

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 Cell Name: esp
 DD-MMM-YYYY HH:MM

Hole 4 C
 Core Log Sta. 361+00, 60' Lt.
 Elev. 818.4-804.9 Overburden
 804.9-796.1 Limestone (Dolomite) tan-brown, granular, weathered, & solutioned, porous, vuggy
 796.1-793.6 Limestone (Dolomite) gray, in shaley matrix
 793.6-792.9 Shale: gray, silty

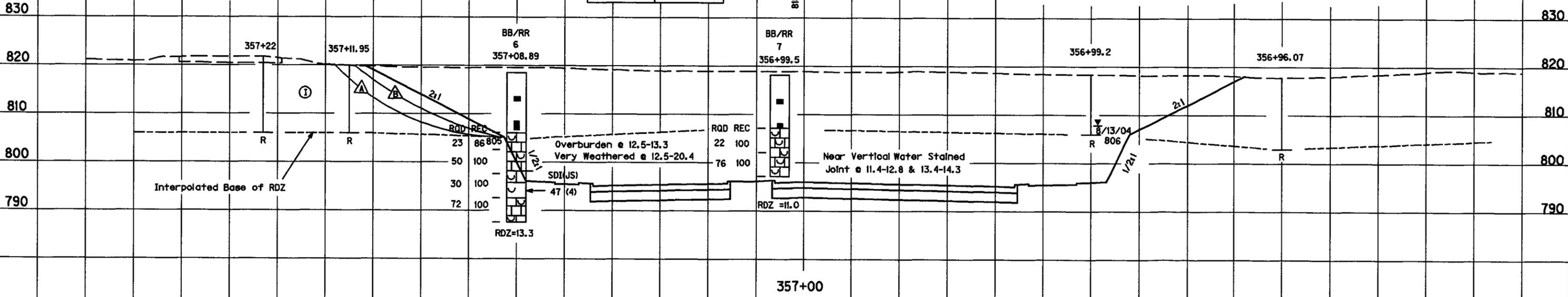


FACTORS OF SAFETY		
INTERMEDIATE TERM	A	2.2
LONG TERM	B	1.4

ASSUMED SOIL STRENGTH PARAMETERS	
SOIL	I
INTERMEDIATE TERM	$\phi = 125$ pof $c = 200$ pcf $\beta = 28^\circ$
LONG TERM	$\phi = 125$ pof $c = 40$ pcf $\beta = 28^\circ$

Hole 6
 Core Log Sta. 357+08.89, 60' Lt.
 Elev. 818.58-806.08 Overburden
 806.08-798.18 Limestone (Dolomite) buff-white-tan, granular, weathered, porous & solutioned
 798.18-795.78 Limestone (Dolomite) gray, fine, crystalline-granular
 795.78-792.58 Shale: gray, clayey, fissile
 792.58-787.58 Limestone (Dolomite) gray, fine-coarse crystalline w/limited shale partings

Hole 7
 Core Log Sta. 356+99.5, 5' Lt.
 Elev. 818.25-807.25 Overburden
 807.25-797.25 Limestone (Dolomite) tan-brown, granular, highly weathered, solutioned, porous w/near vertical fracture set



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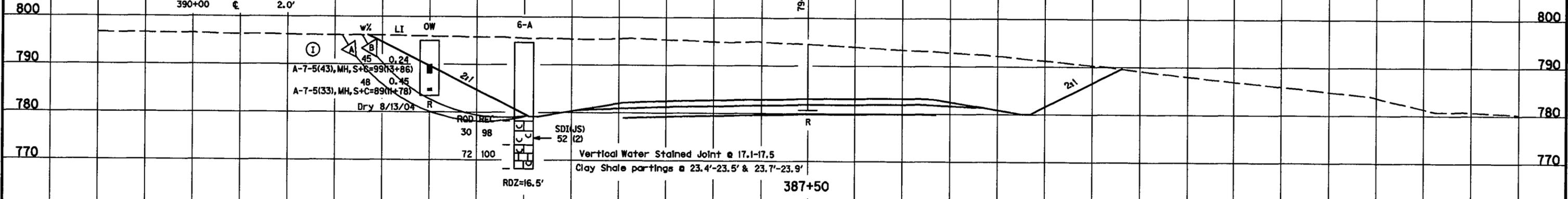
Additional Rockline Soundings

Station	Offset	Depth to Refusal
382+50	45' Lt.	6.5'
383+00	45' Lt.	3.5'
385+50	45' Lt.	8.0'
386+00	40' Lt.	10.0'
387+50	€	14.0'
388+00	58' Lt.	10.0'
388+00	€	14.0'
389+00	58' Lt.	12.5'
389+00	47' Rt.	10.0'
390+00	€	2.0'

FACTORS OF SAFETY		
INTERMEDIATE TERM	A	2.1
LONG TERM	B	1.4

ASSUMED SOIL STRENGTH PARAMETERS	
SOIL	I
INTERMEDIATE TERM	$\phi = 125$ psf $c = 200$ psf $\beta = 28^\circ$
LONG TERM	$\phi = 125$ psf $c = 40$ psf $\beta = 28^\circ$

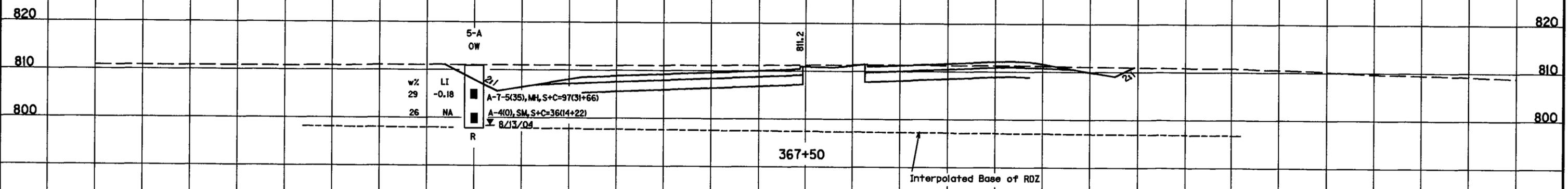
Hole 6 A
 Cut Limits from Sta. 381+50 to Sta. 391+00
 Core Log Sta. 387+50, 60' Lt.
 Elev. 794.5-778.15 Overburden
 778.15-776.15 Limestone : (Dolomite) reddish brown-gray, granular, w/intermittent water staining
 776.15-773.15 Shale : clayey-silty, gray, calcareous
 773.15-768.15 Limestone : (Dolomite) gray, granular w/limited shale partings



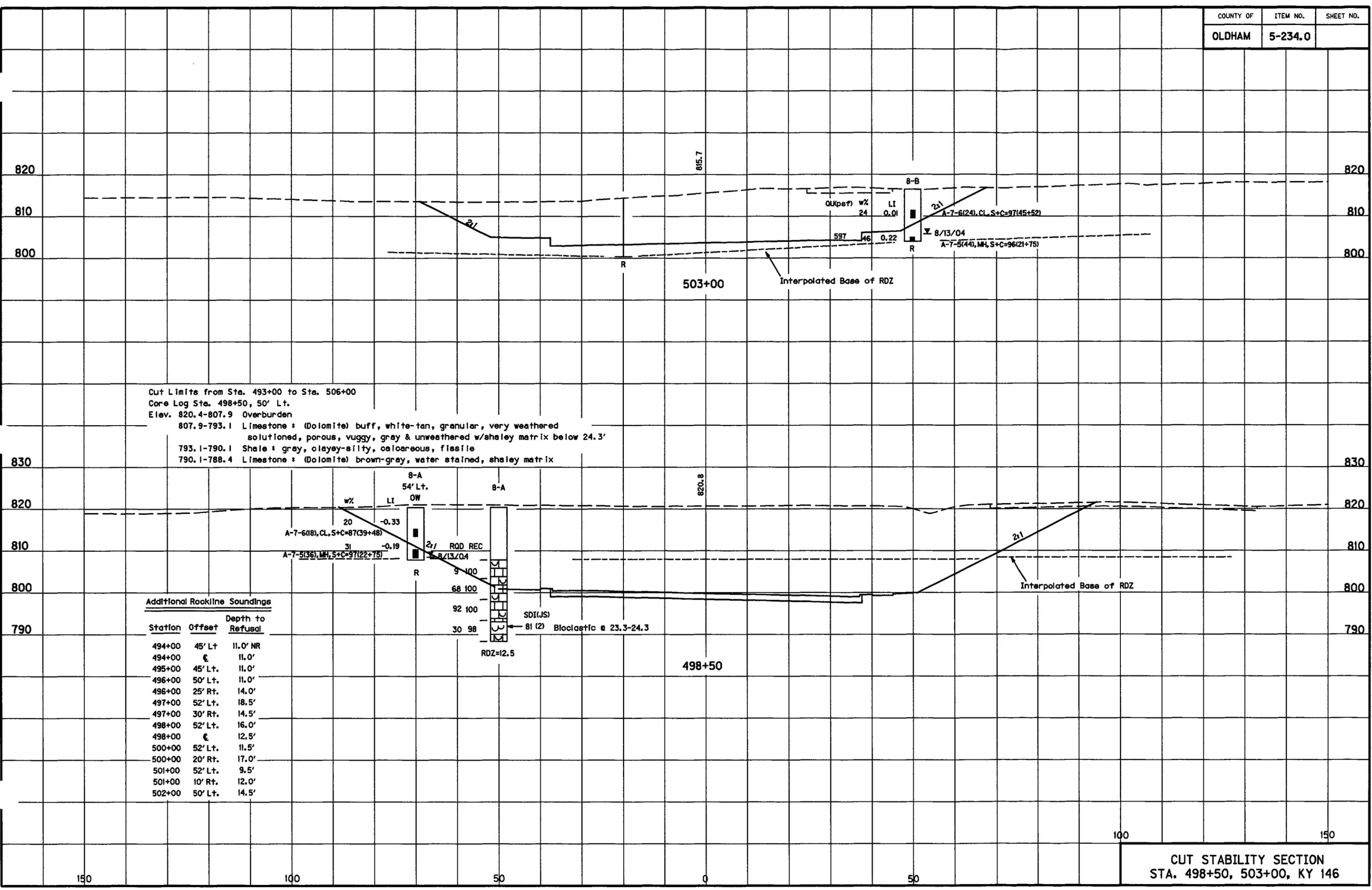
Additional Rockline Soundings

Station	Offset	Depth to Refusal
366+00	70' Lt.	14.5'
367+00	65' Lt.	12.5'

Cut Limits from Sta. 366+00 to Sta. 372+00



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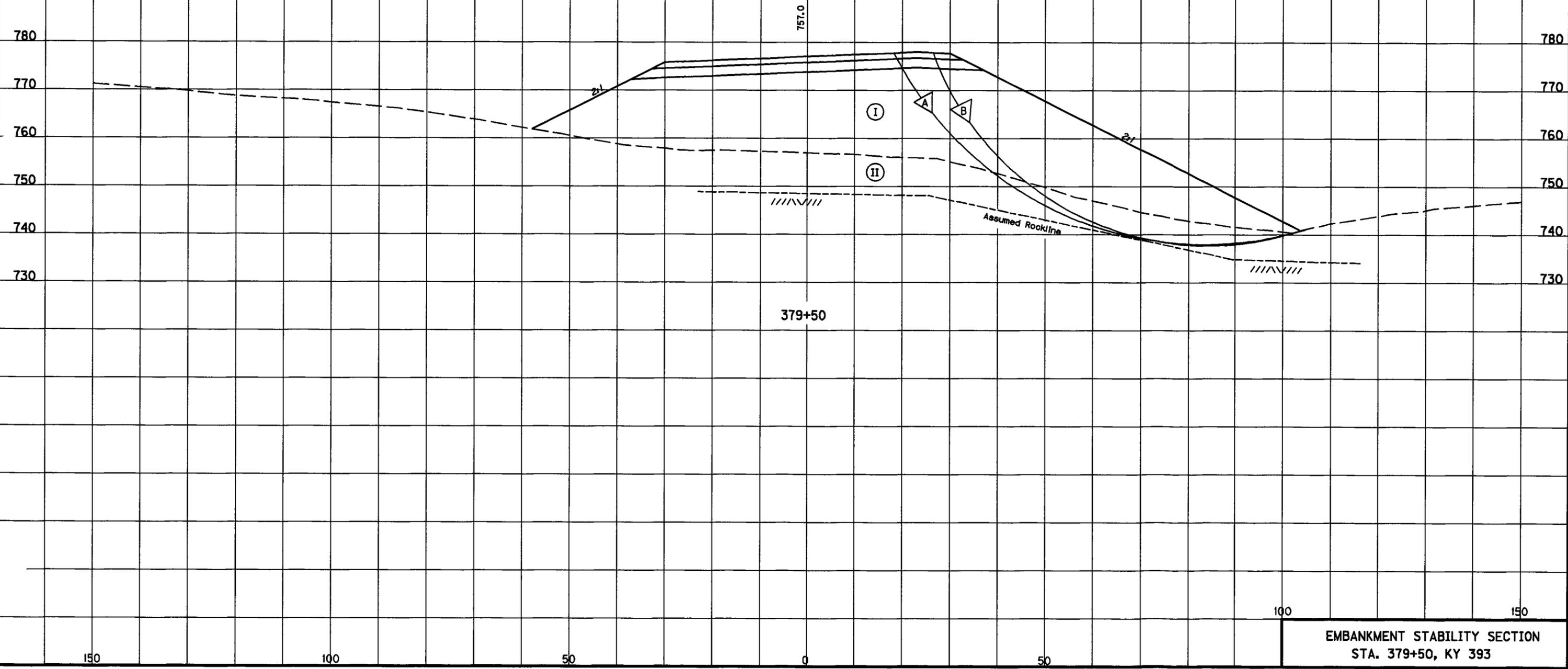


CUT STABILITY SECTION
STA. 498+50, 503+00, KY 146

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FACTORS OF SAFETY		
SHORT TERM	A	2.1
LONG TERM	B	1.4

ASSUMED SOIL STRENGTH PARAMETERS		
SOIL	I	II
SHORT TERM	$\phi = 125$ psf $c = 1500$ psf $\beta = 0^\circ$	$\phi = 125$ psf $c = 1250$ psf $\beta = 0^\circ$
LONG TERM	$\phi = 125$ psf $c = 250$ psf $\beta = 25^\circ$	$\phi = 125$ psf $c = 200$ psf $\beta = 20^\circ$



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 APPROVED BY _____

DUPLICATE THIS SHEET